## NOx REMOVAL IN A CORONA DISCHARGE - CATALYST HYBRID SYSTEM

#### M. Dors, J. Mizeraczyk

#### Centre of Plasma and Laser Engineering, Institute of Fluid Flow Machinery, Polish Academy of Sciences, Fiszera 14, 80-231 Gdańsk, Poland mdors@imp.gda.pl

A b s t r a c t. The objective of this work was to investigate  $NO<sub>x</sub>$  removal employing a hybrid system of a de corona discharge and a catalyst at room temperature (22°C) in the presence of ammonia. Results of the investigation showed that the hybrid system removes up to  $96\%$  of NO<sub>x</sub> with an energy efficiency of 3.4 g NO/kWh. Without the catalyst,  $NO<sub>x</sub>$  decomposition in the "pure" corona discharge with ammonia was lower (up to 66%). Also the energy efficiency was lower (about 1.8 g NO/kWh). The obtained results proved that the investigated hybrid system consisted of the corona discharge and the catalyst is attractive for  $NO_x$  removal because relatively high efficiency both in decomposition and energy.

Key words: corona discharge, catalyst, nitrogen oxides.

### INTRODUCTION

Ten-old years investigations carried out in laboratories and pilot plants showed that removal of  $NO<sub>x</sub>$  from flue gases by corona discharges may be very efficient [1, 2]. However, the energy consumption of this new technology is still not acceptable for commercial use and is to be improved. Thus, many recent investigations have been focused on the performance improvement of the corona discharge process by optimising the power source, using gaseous additives or combining with other methods.

A competitive technology the selective catalytic reduction (SCR) process has proved its efficiency in  $NO<sub>x</sub>$  removal in both selectivity and high performance [3]. In this process, ammonia and a catalyst operating in a relatively high temperature range of 280-430°C are used to reduce NO<sub>x</sub> to N<sub>2</sub> that is harmless product. In the corona disccharge process the dominant mechanism of  $NO<sub>x</sub>$  removal is oxidation to removable HNO<sub>3</sub>, and the selective control of the plasma chemical reaction to reduce  $NO<sub>x</sub>$  to  $N<sub>2</sub>$ , like in the SCR, is difficult. However, in recent years hybrid plasma systems have been proposed because of their capability to decompose  $NO<sub>x</sub>$ 

into  $N_2$  and  $O_2$  [4-9]. A typical hybrid system consists of a corona discharge and a catalyst. So far researchers used a catalyst either as a layer coating the plane electrode in a point-to-plane DC corona discharge reactor [4], or as pellets or globules in a packed bed silent discharge reactors [5-9]. In some hybrid systems, hydrocarbons were added to the air or flue gas polluted with  $NO<sub>x</sub>$  to improve its removal [5, 6, 8]. In the others, ammonia was used as an additive after the corona processing, before the SCR processing [7, 10-12].

The objective of this work was to study  $NO<sub>x</sub>$  removal by a combined system of a DC streamer corona discharge with a catalyst under low temperature (22°C) in the presence of ammonia. In this system ammonia is added to the gas before entering corona discharge reactor.

## EXPERIMENTAL APPARATUS

The non-thermal plasma reactor with the corona discharge and catalyst used in this experiment is shown in Fig. 1. The positive DC corona discharge was generated between a stainless steel hollow needle and a flat mesh (1x1 mm) made of brass. The needle was placed perpendicularly to the mesh. The outer and inner diameter of the needle was 2 mm and 1.6 mm, respectively. The interelectrode distance was varied in the range of 20-40 mm. Gas mixture of  $N_2(80\%)$ : $O_2(5\%)$ : $CO_2(15\%)$ : $NH_3(250ppm)$ : $NO(200ppm)$  flowed through the hollow needle with a flow rate of 1 l/min. The catalyst, typical of the SCR processing, used in the investigation was a mixture of  $V_2O_5$  and  $TiO_2$  deposited on the  $Al_2O_3$  globules of 5-6 mm in diameter. The globules with deposited catalyst were delivered by the Katalizator Co., Krakow, Poland. The catalyst globules were placed on the mesh in the form of 2 or 4 layers, so that the interelectrode distance was always about 40 mm.



Fig. 1. Non-thermal plasma reactor with corona discharge and catalyst.

The positive polarity DC high voltage was applied through a 10  $\text{M}\Omega$  resistor to the hollow needle electrode. The operating voltage was varied from 15 to 38 kV to develop a stable streamer corona discharge. The time averaged discharge current was varied in the range of 50-200 µA. Time dependences of the corona discharge current pulses were measured with a current transformer PEARSON 2878 and recorded on a digital oscilloscope.

Concentrations of NO,  $NO<sub>2</sub>$  and NH<sub>3</sub> in the gas mixture were measured by absorption spectroscopy method using a Perkin-Elmer 16 РС FTIR spectrophotometer operating in the infrared range 4400-1000 cm<sup>-1</sup>.

#### RESULTS

The investigation of  $NO<sub>x</sub>$  abatement by the corona discharge plasma was carried out either in the reactor without catalyst or in the reactor with 2 layers of catalyst globules. In both cases the interelectrode distance was 40 mm. However, when catalyst is present in the reactor, the distance between the catalyst layer and the needle was about 30 mm.

operating gas not containing NF<sub>3</sub> is no inglier than 50% and is accompanied with<br>NO<sub>2</sub> production (Fig. 2a). As a result the NO<sub>x</sub> removal is not higher than 15 % Generally, the removal of NO and  $NO<sub>x</sub>$  increases with increasing corona discharge current. In the case of reactor without catalyst, removal of NO from the operating gas not containing  $NH<sub>3</sub>$  is no higher than 30 % and is accompanied with

(Fig. 2b). NH<sub>3</sub> added to the operating gas increases NO removal and completely removes  $NO<sub>2</sub>$  produced in the corona discharge plasma. However, only small fraction of the introduced  $NH<sub>3</sub>$  is consumed during the corona discharge process. In the presence of the catalyst in the reactor, NO removal from the operating gas without  $NH_3$  is about 50 % and again is accompanied with  $NO_2$  production (Fig. 2a). As a result the  $NO<sub>x</sub>$  removal does not exceed 35 % (Fig. 2b). In the presence of  $NH_3$ , removal of NO and NO<sub>x</sub> increases up to 96% with no production of NO<sub>2</sub> and only 2 ppm of  $NH<sub>3</sub>$  in the outlet gas.

Long time experiment showed that catalyst works stable for about 30 hours (Fig. 3). After that time it loose its activity probably due to covering the globules surface with  $NH_4NO_3$  powder which is formed in the following reaction [10]:

 $(1)$ 

 $(2)$ 

 $2 NO_2 + 2 NH_3 \rightarrow N_2 + H_2O + NH_4NO_3.$ 

From the weight analysis of the  $NH<sub>3</sub>$  and  $NH<sub>4</sub>NO<sub>3</sub>$  one can conclude that only a fraction of  $NO_x$  and  $NH_3$  is transformed into ammonium nitrate. Another reaction responsible for removal of NO<sub>x</sub> and NH<sub>3</sub> is reduction of NO<sub>2</sub> [10]:

 $6 \text{ NO}_2 + 8 \text{ NH}_3 \rightarrow 7 \text{ N}_2 + 12 \text{ H}_2\text{O}.$ 





Concentrations of NO,  $NO_2$ ,  $NO_x$  and  $NH_3$  in the operating gas at the reactor outlet as a Fig. 2. function of time-averaged corona discharge current. Operating gas without and with NH<sub>3</sub> (250 ppm). Catalyst globules formed in 2 layers. Interelectrode distance 40 mm.



Time dependence of NO concentration in the operating gas at the reactor outlet. Operating Fig. 3. gas without and with NH<sub>3</sub> (250 ppm). Catalyst globules formed in 2 layers. Interelectrode distance 40 mm.



Concentrations of NO and  $NO<sub>2</sub>$  in the operating gas at the reactor outlet as a function of  $Fig. 4.$ corona discharge power. Operating gas without and with NH<sub>3</sub> (250 ppm). Catalyst globules formed in 2 layers. Interelectrode distance 40 mm.

The energy consumption during  $NO<sub>x</sub>$  removal process in the corona discharge in the reactor with and without catalyst can be calculated from results presented in Fig. 4. The energy efficiency of the removal of 96% NO in the reactor with catalyst is 3.4 g NO/kWh. This is similar to result obtained by Ohkubo et al. [12] in the corona radical shower reactor with 8 hollow needles. In the case of the reactor without the catalyst (operating gas with  $NH<sub>3</sub>$ , 400 ppm) the energy efficiency of the NO removal is only 1.8 g NO/kWh.

#### **CONCLUSIONS**

The investigation of influence of the catalyst typical for SCR process on  $NO<sub>x</sub>$ removal from the simulated flue gas in the non-thermal corona discharge reactor showed that the catalyst increases substantially  $NO<sub>x</sub>$  removal efficiency. Besides, our hybrid system reduces much energy consumption of  $NO<sub>x</sub>$  removal process what is the main goal of the work. Thus, the obtained results proved that the investigated hybrid system consisted of the corona discharge and the catalyst is attractive for  $NO<sub>x</sub>$  removal and may be alternative to other non-thermal plasma methods of gas cleaning.

## ACKNOWLEDGMENT

This work was supported by the Institute of Fluid Flow Machinery, Polish Academy of Sciences, Gdańsk (grant IMP PAN O3/Z-3/T2).

## REFERENCES

- Chang J.S., in: Non-thermal Plasma Techniques for Pollution Control, Eds. B.M. Penetrante and 1. S.E. Schultheis, Springer-Verlag Berlin Heidelberg, NATO ASI Series, 1993, vol. G 34 (A), pp. 1-32.
- $\overline{2}$ . Van Veldhuizen E. M., Electrical Discharges for Environmental Purposes, Nova Science Publishers, New York, 2000.
- $3.$ Hjalmarsson A.K., Int. J. of Ener. Res. 14, 813-820, 1990.
- $3.4.5.6.7.8.$  $4.$ Suhr H., Weddigen G., Combust. Sci. Technol. 72, 101-115, 1990.
- Shimizu K., Oda T., IEEE Trans. Ind. Appl. 35, 1311-1318, 1999. 5.
- Oda T., Kato T., Takahashi T., Shimizu K., J. Electrostatics 42, 151-157, 1997. 6.
- Kim H.H., Takashima K., Katsura S., Mizuno A., J.Phys. D: Appl. Phys. 34, 604-613, 2001. 7.
- 8. Yamamoto T., Yang C.-L., Beltran M. R., Kravets Z., IEEE Ind. Appl. Society Annual Meeting, New Orleans, USA, pp. 1956-1960, 1997.
- o Kawasaki T., Kanazawa S., Ohkubo T., Mizeraczyk J., Nomoto Y., Thin Solid Films 386, 177-182, 2001.
- 10. Hammer T., Broer S., Plasma Enhanced Selective Catalytic Reduction of NO<sub>v</sub> for Diesel Cars, Society of Automotive Engineers Technical Paper Series, No. 982428, 1998.
- . Hammer T., Kishimoto T., Miessner H., Rudolph R., Plasma Enhanced Selective Catalytic Reduction: Kinetics of NO, Removal and Byproducts Formation, Society of Automotive Engineers Technical Paper Series, No. 1999-01-3632, 1999.
- 12. Ohkubo T., Kanazawa S., Nomoto Y., Chang J.S., Adachi T., IEEE Trans. Ind. Appl. 30, 856-860, 1994.

# ELIMINACJA NOx W UKŁADZIE HYBRYDOWYM WYŁADOWANIE KORONOWE — KATALIZATOR

#### M. Dors, J. Mizeraczyk

#### Ośrodek Techniki Plazmowej i Laserowej, Instytut Maszyn Przepływowych PAN, 80-231 Gdańsk, Fiszera 14, Polska mdors@imp.gda.pl

Streszczenie. Tematem pracy było badanie procesu eliminacji NO<sub>x</sub> w układzie hybrydowym DC wyładowanie koronowe — katalizator w temperaturze pokojowej (22 ° C) w obecności amoniaku. Uzyskano efektywność usuwania do 96% NO, przy efektywności energetycznej 3.4 g NO/kWh. W procesie bez katalizatora stopień eliminacji  $NO<sub>x</sub>$  był niższy (do 66%), jak również efektywność energetyczna (ok. 1.8 gNO/kWh). Otrzymane rezultaty wskazują na atrakcyjność systemu hybrydowego z powodu wysokiego stopnia eliminacji NO<sub>x</sub> i wykorzystania energii.

Słowakluczowe: wyładowania koronowe, kataliza, tlenki azotu.